

**Optimum Short-Term Hydrothermal
Scheduling with Spinning Reserve
through Network Flows.**

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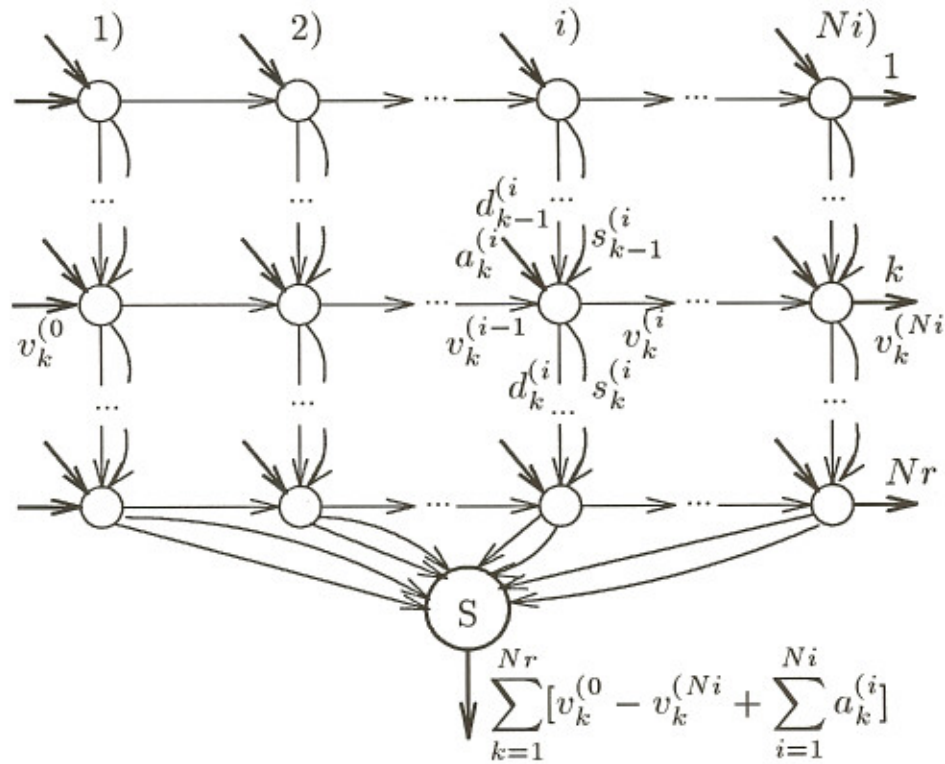
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DESCRIPTION OF THE PROBLEM

- **Given :**
 - * A hydro system with N_r reservoirs.
 - * A thermal system with N_u thermal units.
 - * A set of N_l load nodes.
 - * A transmission network.
 - **find, for each time interval of the period studied:**
 - * The reservoir discharges and storages.
 - * The thermal unit power output.
 - * The power flows on the transmission network.
 - **such that minimize:**
 - * The thermal generation cost.
 - * The losses on the transmission network.
 - **satisfying:**
 - * The forecasted load requirements.
 - * The spinning reserve requirements.
 - * The KCL and KVL in the transmission network.
-

HYDRO NETWORK



- Balance equation at reservoir k over interval i :

$$a_k^{(i)} + v_k^{(i-1)} + d_{k-1}^{(i)} + s_{k-1}^{(i)} = v_k^{(i)} + d_k^{(i)} + s_k^{(i)} \quad (1)$$

(delays and pumping are considered but not depicted here)

HYDROGENERATION FUNCTION

- **Hydrogeneration at reservoir k over interval i :**

$$H_k^{(i)} = \mu \rho_k^{(i)} h_k^{(i)} d_k^{(i)} \quad (2)$$

- * Reservoir head function :

$$h_k = s_{bk} + s_{lk} v_k + s_{qk} v_k^2 + s_{ck} v_k^3 \quad (3)$$

- * Efficiency :

$$\begin{aligned} \rho_k^{(i)} = & \rho_{k0} + \rho_{kh} h_k^{(i)} + \rho_{kd} d_k^{(i)} + \\ & + \rho_{khd} h_k^{(i)} d_k^{(i)} + \rho_{khh} (h_k^{(i)})^2 + \rho_{kdd} (d_k^{(i)})^2 \end{aligned} \quad (4)$$

- **Total hydrogeneration over interval i :**

$$H^{(i)} = \sum_{k=1}^{Nr} H_k^{(i)} \quad (5)$$

- **Hydrogeneration linearization :**

$$H_k^{(i)} \approx H_{Lk}^{(i)} = \lambda_{0k}^{(i)} + \lambda_{v(i-1)k}^{(i)} v_k^{(i-1)} + \lambda_{v(i)k}^{(i)} v_k^{(i)} + \lambda_{dk}^{(i)} d_k^{(i)} \quad (6)$$

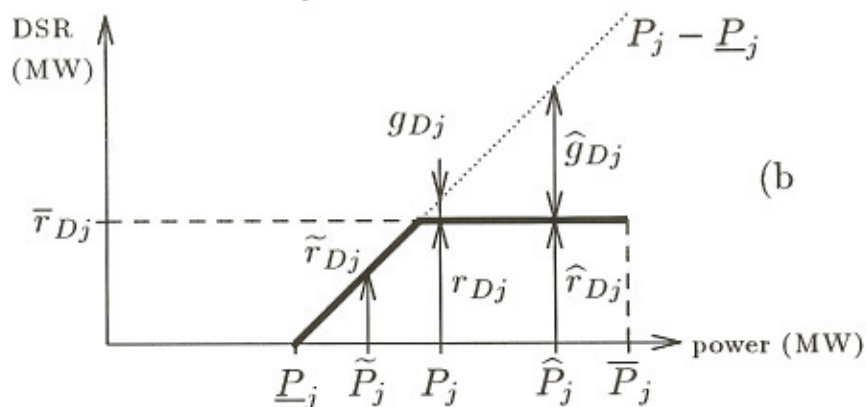
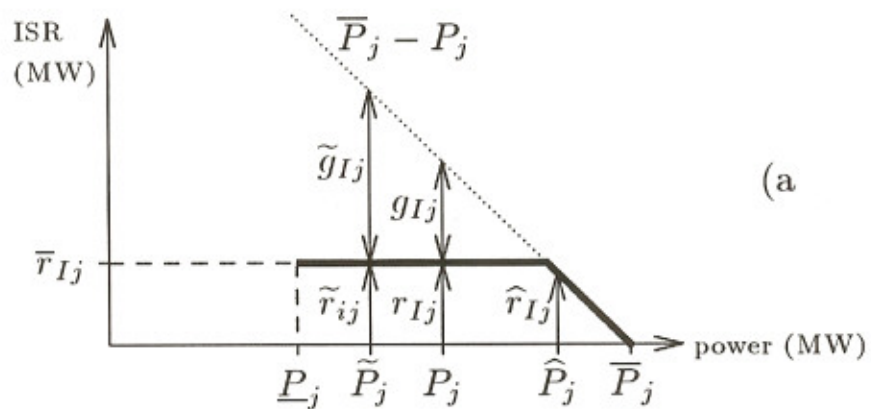
THERMAL SYSTEM MODELIZATION

- Variables associated to the generation of a single unit:

$$\underline{P}_j \leq P_j \leq \bar{P}_j \tag{7}$$

$$r_{Ij} = \min\{\bar{r}_{Ij}, \bar{P}_j - P_j\} \tag{8}$$

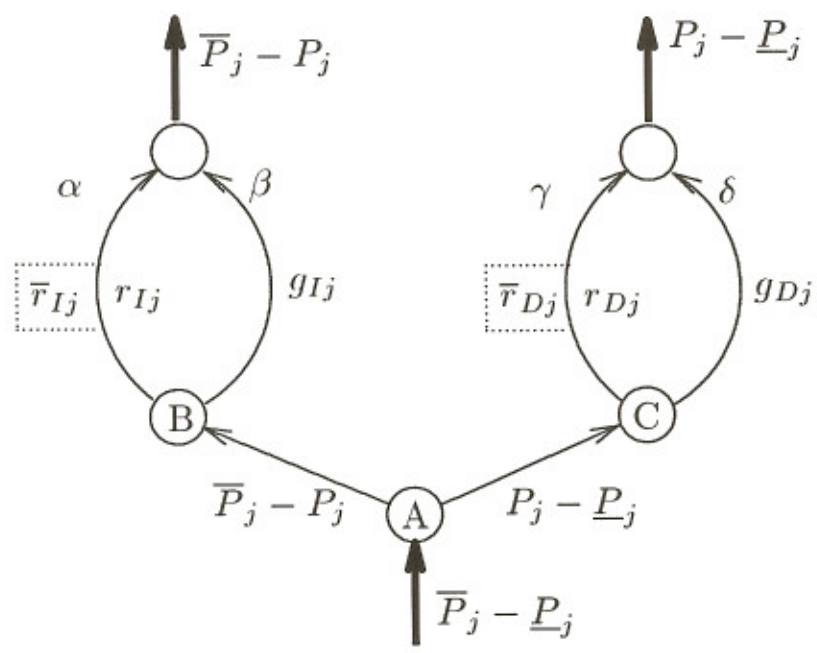
$$r_{Dj} = \min\{\bar{r}_{Dj}, P_j - \underline{P}_j\} \tag{9}$$

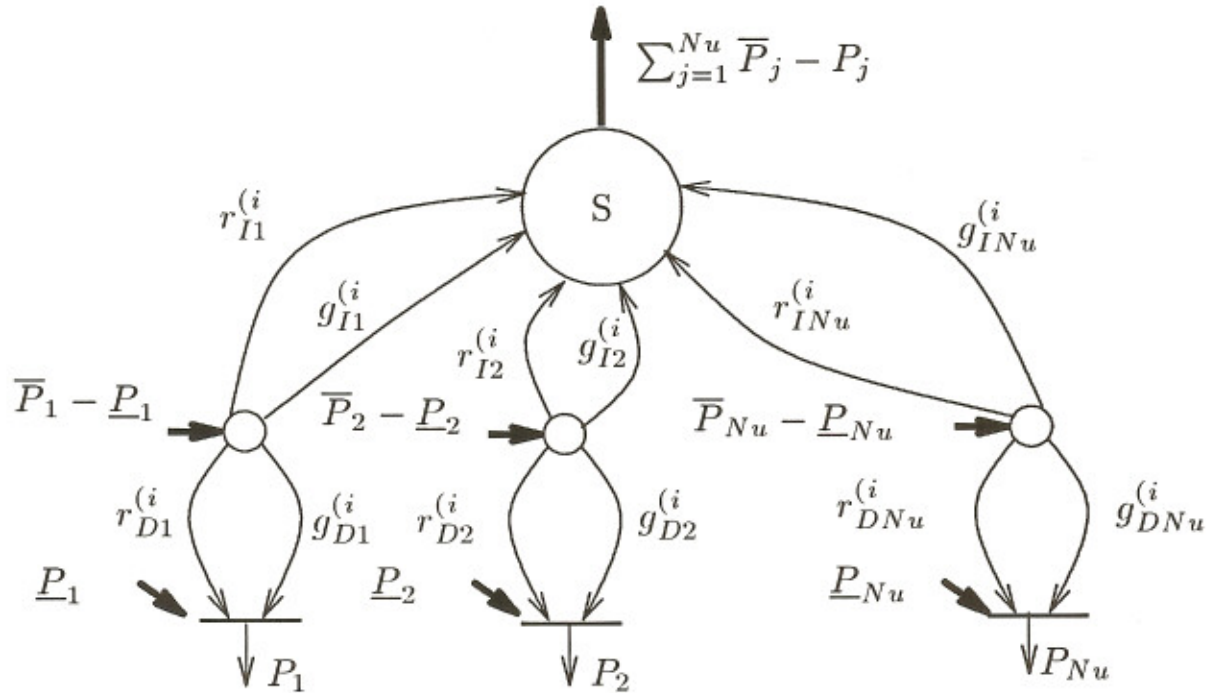


EQUIVALENT THERMAL NETWORK UNIT j

$$r_{Ij} \leq \min\{\bar{r}_{Ij}, \bar{P}_j - P_j\} \begin{cases} r_{Ij} \leq \bar{r}_{Ij} & (10) \\ r_{Ij} \leq \bar{P}_j - P_j \\ \downarrow \\ r_{Ij} + g_{Ij} = \bar{P}_j - P_j & (11) \end{cases}$$

$$r_{Dj} \leq \min\{\bar{r}_{Dj}, P_j - \underline{P}_j\} \begin{cases} r_{Dj} \leq \bar{r}_{Dj} & (12) \\ r_{Dj} \leq P_j - \underline{P}_j \\ \downarrow \\ r_{Dj} + g_{Dj} = P_j - \underline{P}_j & (13) \end{cases}$$



THERMAL SYSTEM NETWORK AT INTERVAL i


- **Balance equations :**

$$* \bar{P}_j - \underline{P}_j = r_{Ij}^{(i)} + g_{Ij}^{(i)} + r_{Dj}^{(i)} + g_{Dj}^{(i)} \quad j = 1, \dots, Nu \quad (14)$$

- **Thermal generation at interval i :**

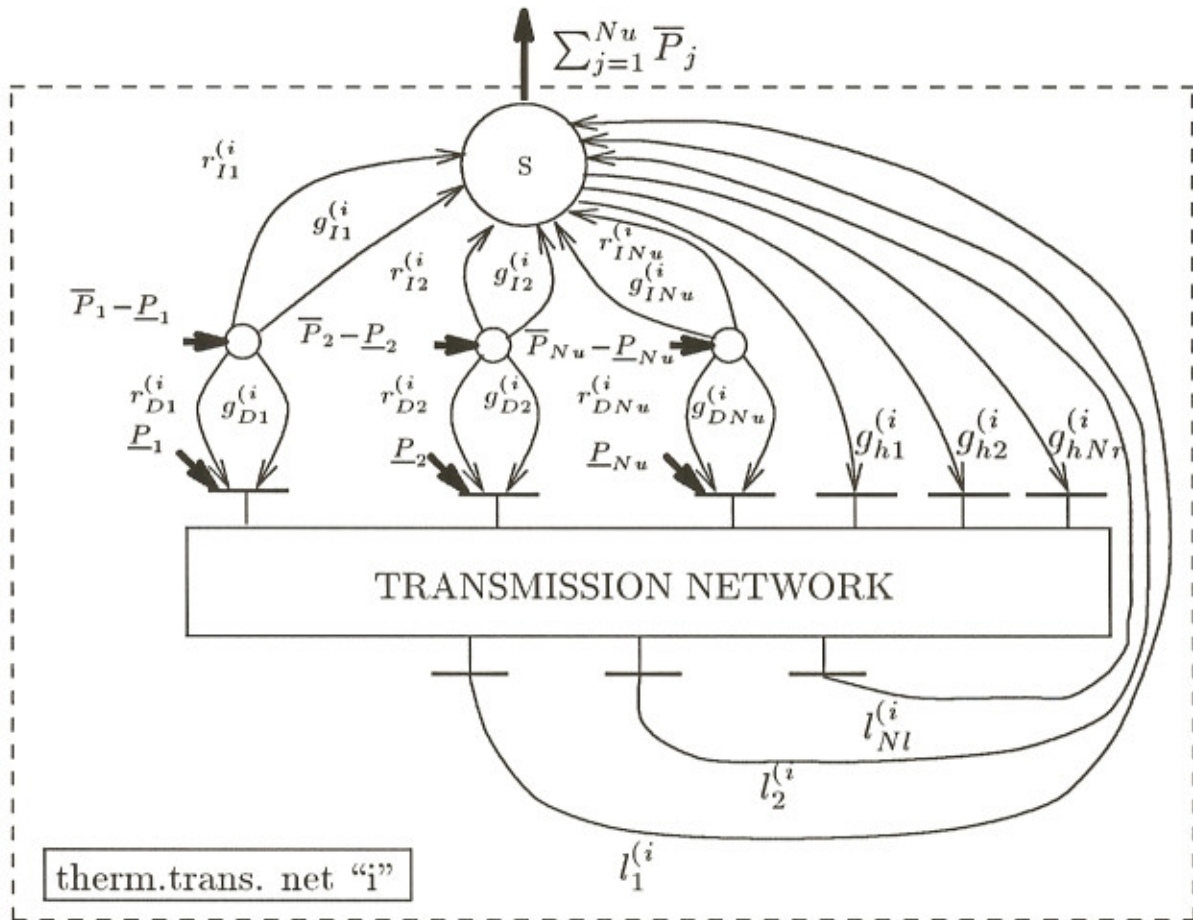
$$* P^{(i)} = \sum_{j=1}^{Nu} (r_{Dj}^{(i)} + g_{Dj}^{(i)} + \underline{P}_j) \quad (15)$$

- **Spinning reserve at interval i : (underestimate)**

$$* \text{Incremental : } \sum_{j=1}^{Nu} r_{Ij}^{(i)} \quad (16)$$

$$* \text{Decremental : } \sum_{j=1}^{Nu} r_{Dj}^{(i)} \quad (17)$$

THERMAL + TRANSMISSION NETWORK

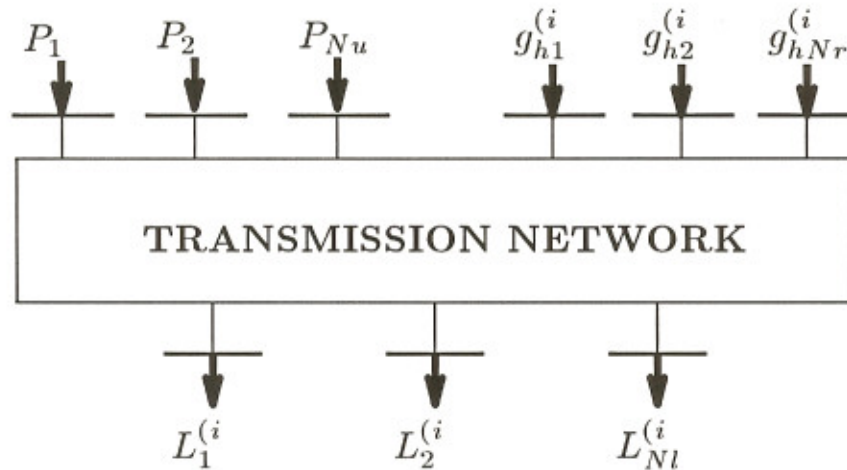


- Hydrogeneration arcs flow equal to the hydrogeneration value :

$$g_{hk}^{(i)} = H_k^{(i)} \approx \lambda_{0k}^{(i)} + \lambda_{v^{(i-1)k}}^{(i)} v_k^{(i-1)} + \lambda_{v^{(i)k}}^{(i)} v_k^{(i)} + \lambda_{dk}^{(i)} d_k^{(i)} \quad k = 1, \dots, Nr \quad (18)$$

- Load arcs :

$$L_l^{(i)} - \epsilon \leq l_l^{(i)} \leq L_l^{(i)} + \epsilon \quad l = 1, \dots, Nl \quad (19)$$

TRANSMISSION NETWORK AT INTERVAL i 

- dc approach considered.
- Line capacity :

$$-\bar{p}_m \leq p_m^{(i)} \leq \bar{p}_m, \quad m = 1, \dots, Nm$$

- Kirchhoff's laws :

* KCL : balance equations of the transmission network.

* KVL :

$$\sum_{m \in C_j} X_m p_m^{(i)} = 0 \quad ; \quad j = 1, \dots, Nc \quad (20)$$

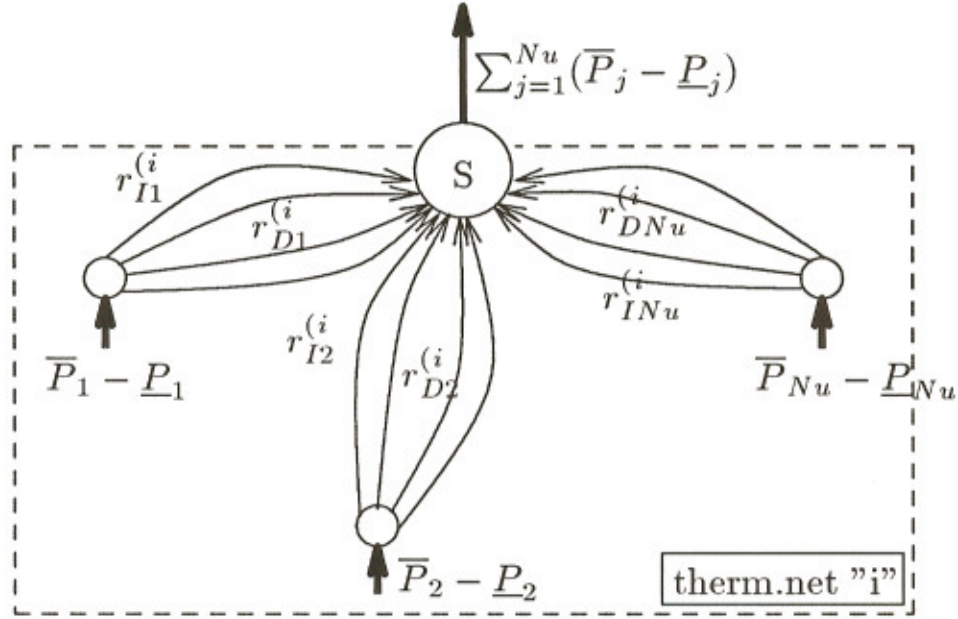
Nc : number of basic loops.

C_j : lines belonging to the j^{th} basic loop.

X_j : line reactance (p.u.).

THERMAL NETWORK AT INTERVAL i

(without transmission network)



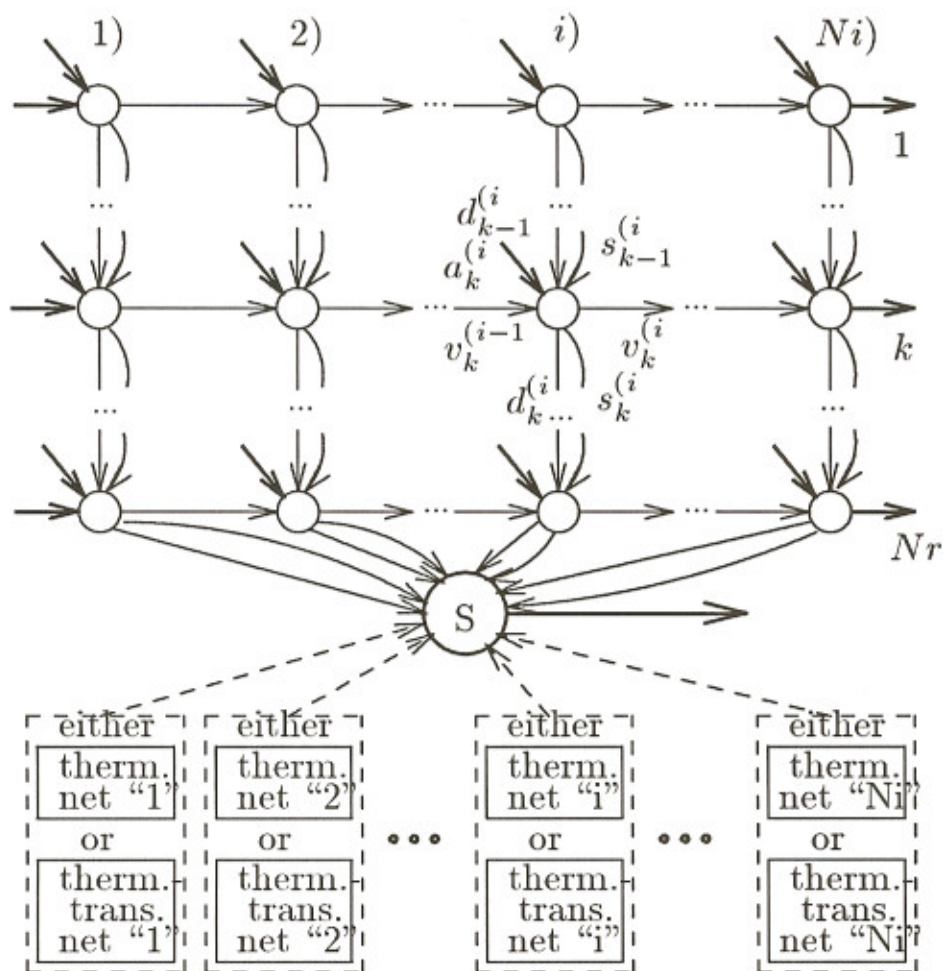
- Load side constraint :

$$\sum_{k=1}^{Nr} H_k^{(i)} + \sum_{j=1}^{Nu} (r_{Dj}^{(i)} + g_{Dj}^{(i)} + \underline{P}_j) = L^{(i)} \quad (21)$$

- * If linearized hydrogeneration is considered :

$$\sum_{k=1}^{Nr} \lambda_{0k}^{(i)} + \lambda_{v(i-1)k}^{(i)} v_k^{(i-1)} + \lambda_{v(i)k}^{(i)} v_k^{(i)} + \lambda_{dk}^{(i)} d_k^{(i)} + \sum_{j=1}^{Nu} (r_{Dj}^{(i)} + g_{Dj}^{(i)} + \underline{P}_j) = L^{(i)} \quad (22)$$

HYDRO-THER.-TRANS. EXT. NET. (HTTEN)



VARIABLES AND OBJECTIVE FUNCTION

- **Variables :** $i = 1, \dots, Ni$
 - * Hydro variables : $d_k^{(i)}, s_k^{(i)}, v_k^{(i)}, k = 1, \dots, Nr$
 - * Thermal variables : $r_{Ij}^{(i)}, g_{Ij}^{(i)}, r_{Dj}^{(i)}, g_{Dj}^{(i)}, j = 1, \dots, Nu$
 - * Transmission variables : $p_m^{(i)}, m = 1, \dots, Nm$
 - * Hydrogen. variables : $g_{hj}^{(i)}, j = 1, \dots, Nr$

- **Objective function : two parts**

- * Thermal generation costs :

$$\sum_{i=1}^{Ni} \sum_{j=1}^{Nu} [c_{lj}(r_{Dj}^{(i)} + g_{Dj}^{(i)} + \underline{P}_j) + c_{qj}(r_{Dj}^{(i)} + g_{Dj}^{(i)} + \underline{P}_j)^2] \quad (23)$$

- * Costs of power losses:

$$\sum_{i=1}^{Ni} \pi^{(i)} \sum_{m=1}^{Nm} r_m (p_m^{(i)})^2 \quad (24)$$

$$\min \sum_{i=1}^{Ni} \left\{ \sum_{j=1}^{Nu} [c_{lj}(r_{Dj}^{(i)} + g_{Dj}^{(i)} + \underline{P}_j) + c_{qj}(r_{Dj}^{(i)} + g_{Dj}^{(i)} + \underline{P}_j)^2] + \pi^{(i)} \sum_{m=1}^{Nm} r_m (p_m^{(i)})^2 \right\} \quad (25)$$

CONSTRAINTS

- **Balance equations of th HTTEN.**
- **Side constraints : for each interval : $i = 1, \dots, Ni$**
 - * Hydrogeneration arcs flow equal to the hydrogeneration value :

$$g_{hk}^{(i)} = H_k^{(i)} \approx \lambda_{0k}^{(i)} + \lambda_{v(i-1)k}^{(i)} v_k^{(i-1)} + \lambda_{v(i)k}^{(i)} v_k^{(i)} + \lambda_{dk}^{(i)} d_k^{(i)} \quad k = 1, \dots, Nr \quad (18)$$

- * Incremental spinning reserve :

$$\sum_{k=1}^{Nr} (\bar{H}_k^{(i)} - g_{hk}^{(i)}) + \sum_{j=1}^{Nu} r_{Ij}^{(i)} \geq R_I^{(i)} \quad (26)$$

- * Decremental spinning reserve :

$$\sum_{k=1}^{Nr} g_{hk}^{(i)} + \sum_{j=1}^{Nu} r_{Dj}^{(i)} \geq R_D^{(i)} \quad (27)$$

- * KVL :

$$\sum_{m \in \mathcal{C}_j} X_m p_m^{(i)} = 0 \quad ; \quad j = 1, \dots, Nc \quad (20)$$

- **Variable bounds.**

OPTIMIZATION PROBLEM

- **Exact hydrogenation function :**

$$\begin{array}{l}
 \text{(NNNC)} \left\{ \begin{array}{ll}
 \min & f(x) & (28a) \\
 \text{subj. to :} & Ax = r & (28b) \\
 & g(x) + \mathbf{I}_z z = b & (28c) \\
 & 0 \leq x \leq u_x & (28d)
 \end{array} \right.
 \end{array}$$

- **Linearized hydrogenation function :**

$$\begin{array}{l}
 \text{(NNLC)} \left\{ \begin{array}{ll}
 \min & f(x) & (29a) \\
 \text{subj. to :} & Ax = r & (29b) \\
 & Tx + \mathbf{I}_z z = b & (29c) \\
 & 0 \leq x \leq u_x & (29d)
 \end{array} \right.
 \end{array}$$

SOLUTION METHODS

- (NNLC) problem : NOXCB (Heredia & Nabona)
 - * Specialised code for the nonlinear network flow problem with linear side constraints :

$$g_{hk}^{(i)} = \lambda_{0k}^{(i)} + \lambda_{v^{(i-1)k}}^{(i)} v_k^{(i-1)} + \lambda_{v^{(i)k}}^{(i)} v_k^{(i)} + \lambda_{dk}^{(i)} d_k^{(i)} \quad (18)$$

- * Successive linearizations.
 - * Any other set of linear constraint could be included.
- (NNNC) problem : MINOS (Murtagh & Saunders)
 - * General purpose nonlinear optimization package :

$$g_{hk}^{(i)} = \mu \rho_k^{(i)} h_k^{(i)} d_k^{(i)}$$

ITERATIVE SOLUTION METHOD

0 Initializations.**0.1** Definition of the network equations of (NNLC)⁰**0.2** Selection of the initial solution $[x]^0$; $k := 1$.**0.3** Maximum hydrogeneration error : $\epsilon_L \approx 0.02$ **1** Major iterations.**1.4** Linearization about $[x]^{k-1} \rightarrow$ (NNLC)^k.**1.5** Optimization of (NNLC)^k with NOXCB $\rightarrow [x]^k$ **1.6** If $|[H_L^{(i)}]^k - [H^{(i)}]^k| < \epsilon_L L^{(i)}, \forall i$ then $x^* := [x]^k$; STOP**1.7** $k := k + 1$. go to **1.4** .

COMPUTATIONAL RESULTS

Table I : Case examples

Problem ident.	Power system size					Opt. problem size		
	Nr	Nu	Nm	Nb	Ni	arcs	nodes	S.C.
A24	3	4	-	-	24	648	163	72
A48	3	4	-	-	48	1248	313	144
A168	3	4	-	-	168	4536	1135	504
B48	6	4	-	-	48	1824	457	144
B168	6	4	-	-	168	6552	1639	504
B48x	6	4	6	5	48	2256	697	240
B168x	6	4	6	5	168	8064	2479	840
C48	9	8	19	12	48	4416	1346	528
C168	9	8	19	12	168	15600	4741	1848

Table II : Computational results

Problem ident.	max. gen. err.	no. of linear.	CPU (s) ¹		Cost (10 ⁶ Pts)	
			NOXCB	MINOS	NOXCB	MINOS
A24	$\leq 0.7\%$	3	14.7	38.7	73.10	73.15
A48	$\leq 1.1\%$	3	39.2	219.6	124.23	124.39
A168	$\leq 1.4\%$	3	623.5	6530.7	361.82	362.16
B48	$\leq 0.9\%$	3	31.2	514.3	123.07	123.19
B168	$\leq 1.5\%$	2	336.2	6667.8	361.30	361.62
B48x	$\leq 1.3\%$	3	49.5	394.1	132.15	132.34
B168x	$\leq 1.4\%$	2	538.4	4963.2	384.40	384.54
C48	$\leq 1.5\%$	2	337.6	6020.1	199.32	199.47
C168	$\leq 1.7\%$	2	2982.47	—	538.73	—

¹ SUN SparcStation 10/41.

B48x : LOAD COVERAGE

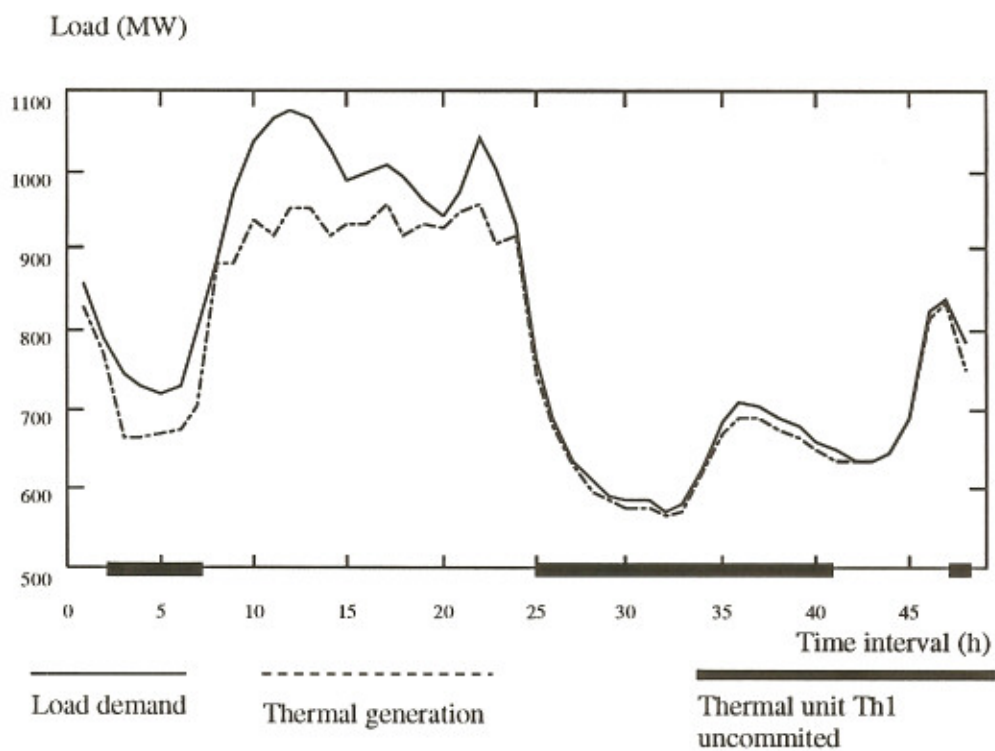


Fig. 1 Attainment of load at the optimal solution of case B48x.

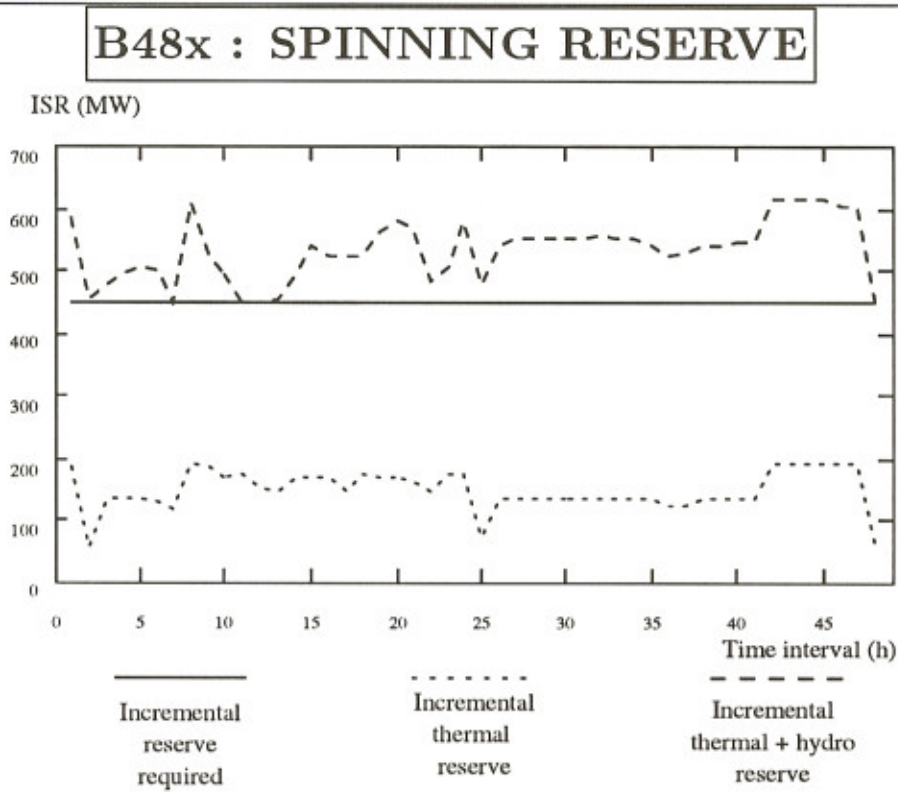


Fig. 2 Incremental reserve at the optimal solution of case B48x.

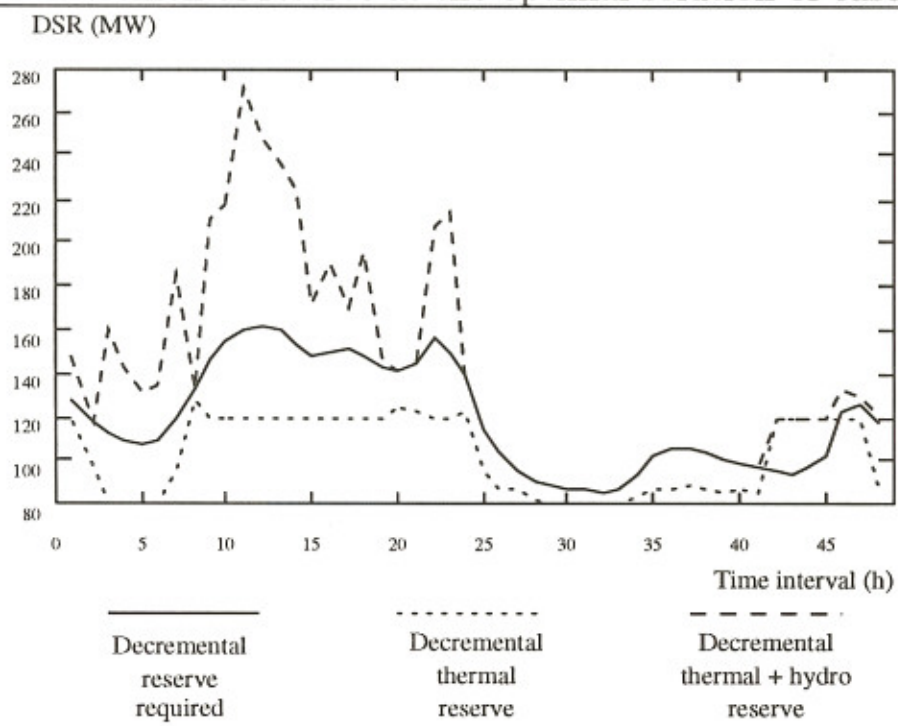


Fig. 3 Decremental reserve at the optimal solution of case B48x.

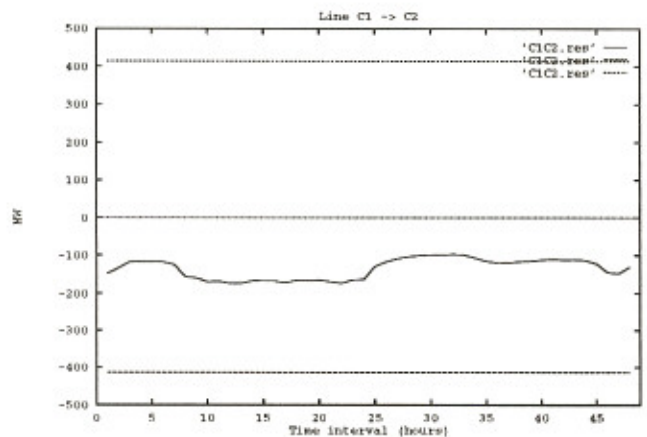
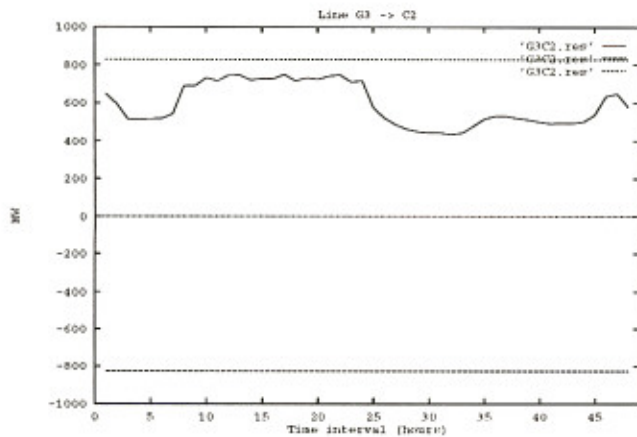
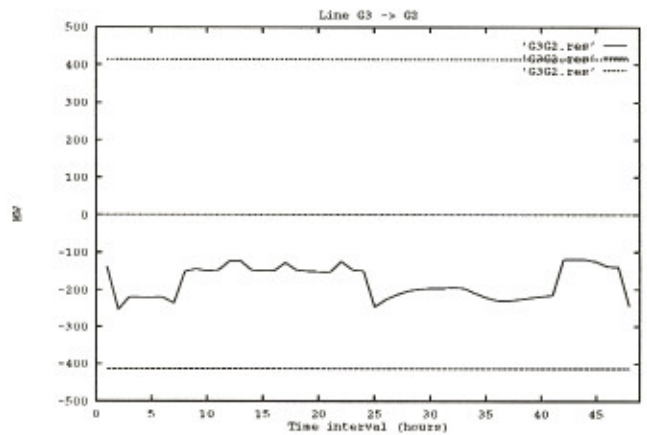
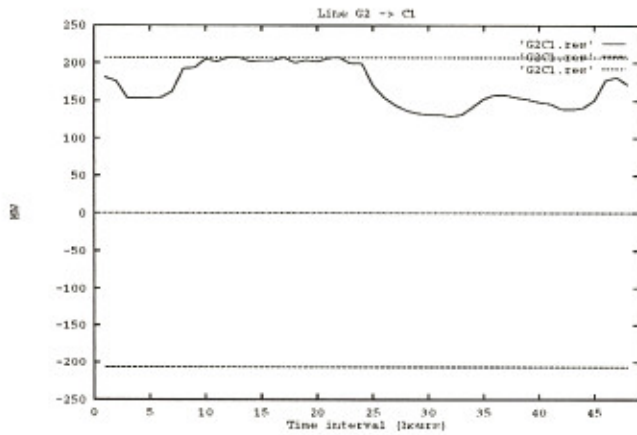
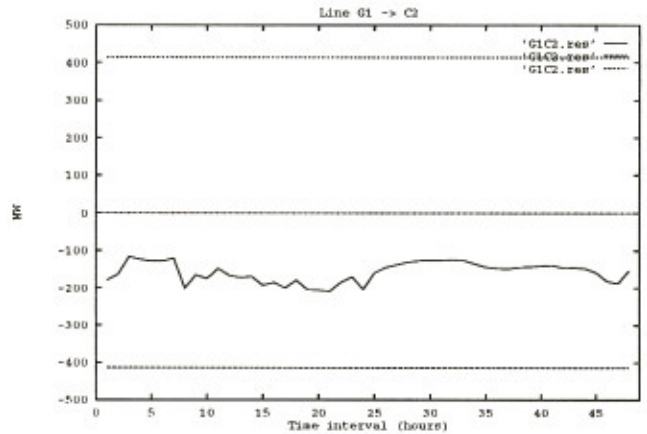
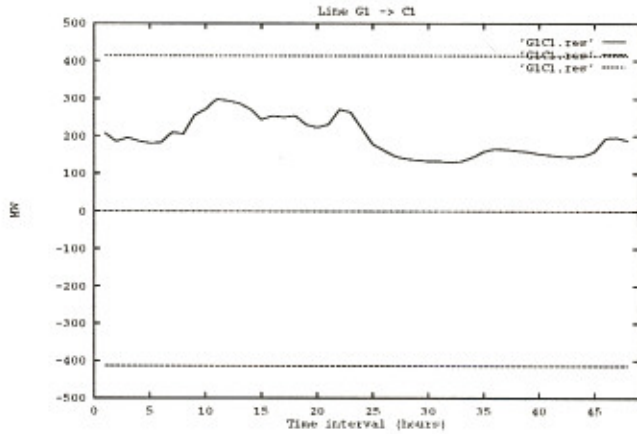
CONCLUSIONS

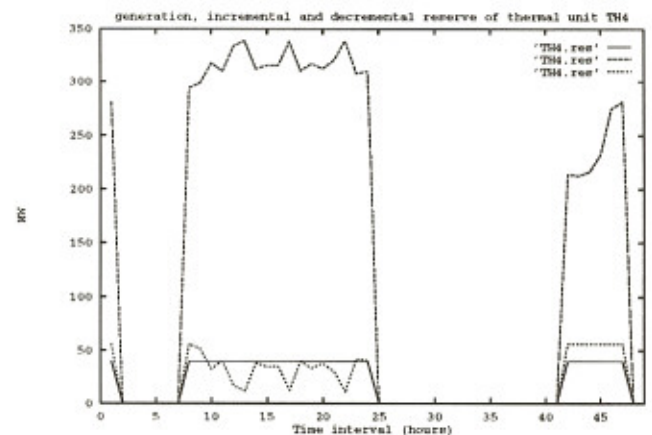
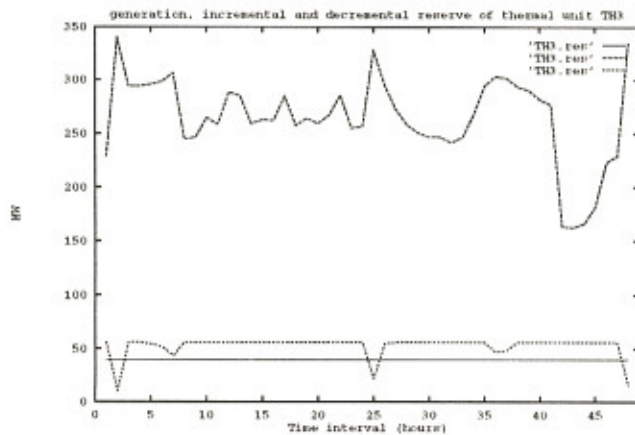
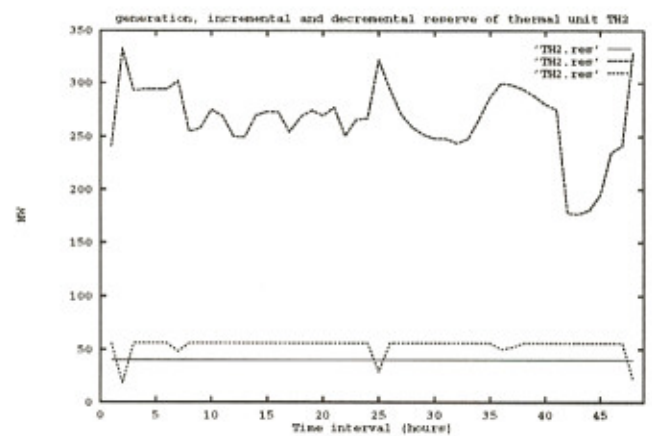
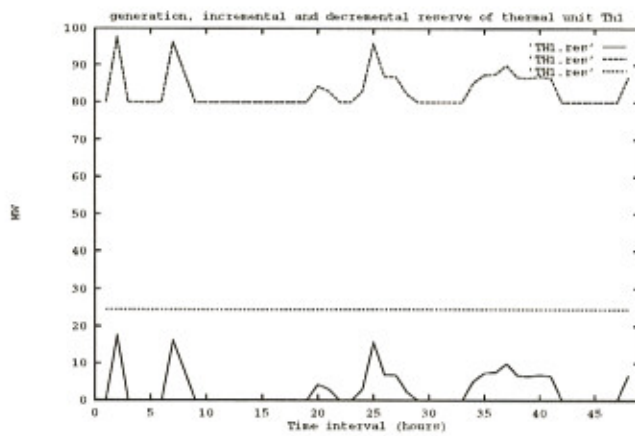
- **Thermal equivalent network :**
 - * Network flow model for the thermal generation and spinning reserve.
 - **Coupled model :**
 - * Optimization of generation costs and trans. losses.
 - * HTTEN : Hydro, thermal and trans. network.
 - * Coupling constraints : hydrogeneration arcs and spinning reserve.
 - * Multi-interval hydrothermal dc OPF.
 - **Successive linearizations :**
 - * ~ one order of magnitude faster.
 - * Deviation from the exact optimum : < 0.14%.
 - * Hydrogeneration linearization error : < 2%.
-

FURTHER DEVELOPMENTS

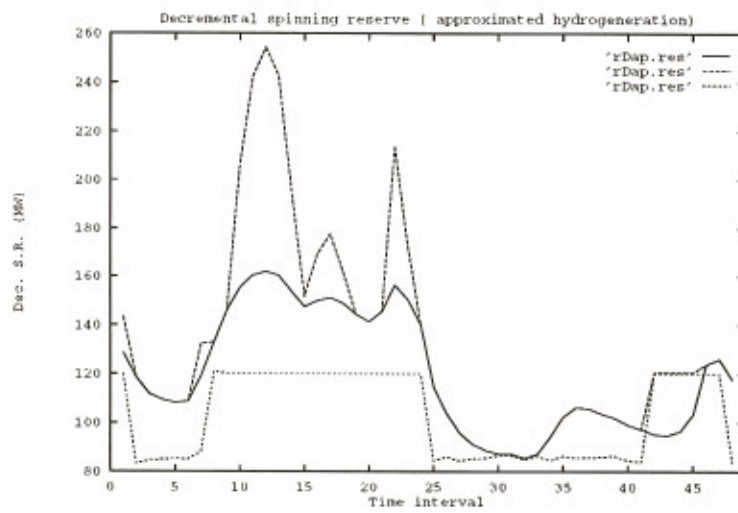
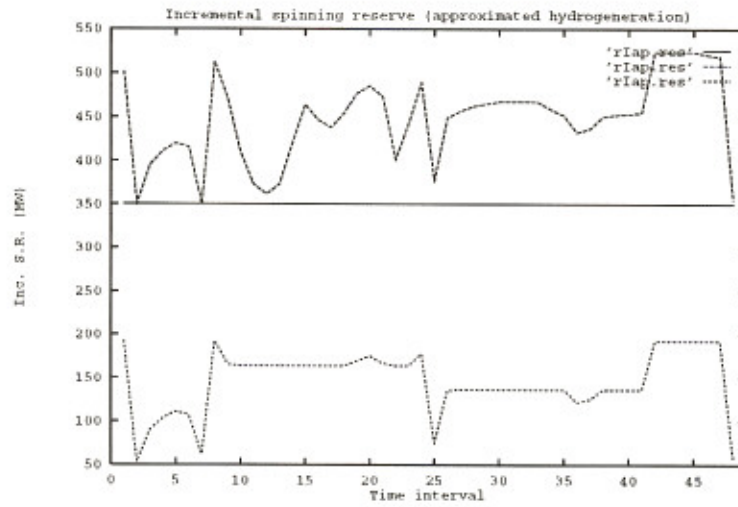
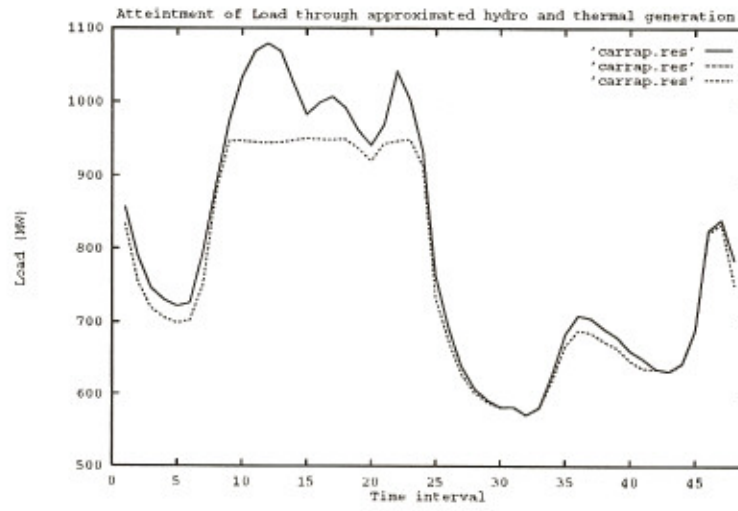
- **Practical interest of the model:**
 - * Experiments with bigger power systems.
 - * Coupled model vs. decoupled model with equivalent thermal network.
 - **Extensions of the coupled model :**
 - * Security constraints.
 - * ac OPF.
 - * Unit commitment.
 - **Extensions of the solution methods :**
 - * Extension of NOXCB to treat nonlinear constraints.
-

B48x : TRANSMISSION LINES

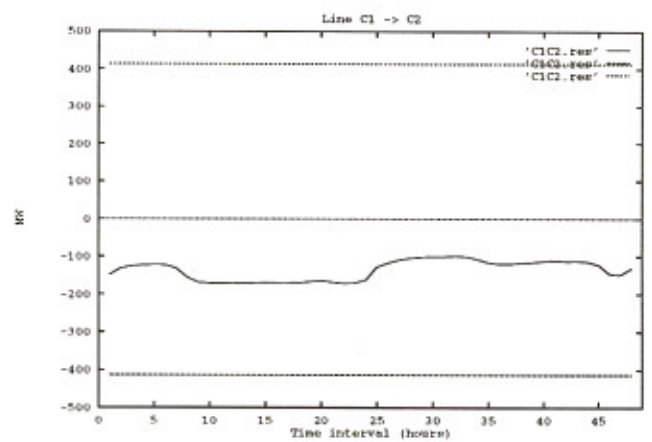
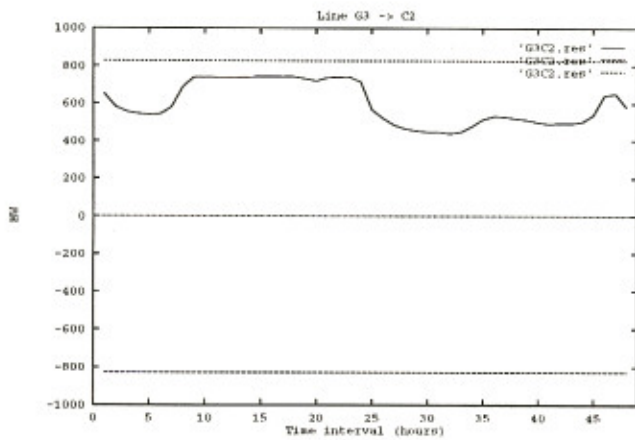
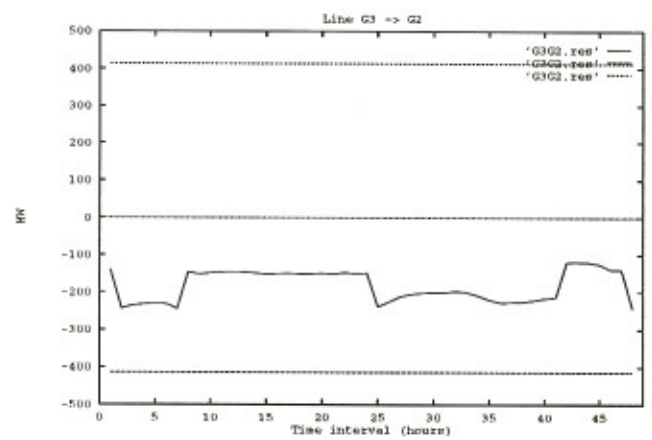
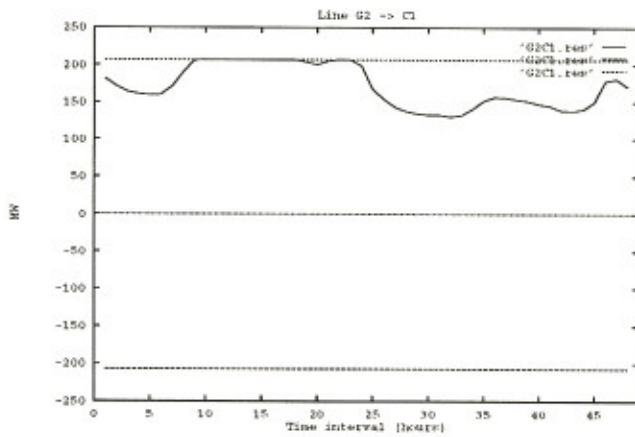
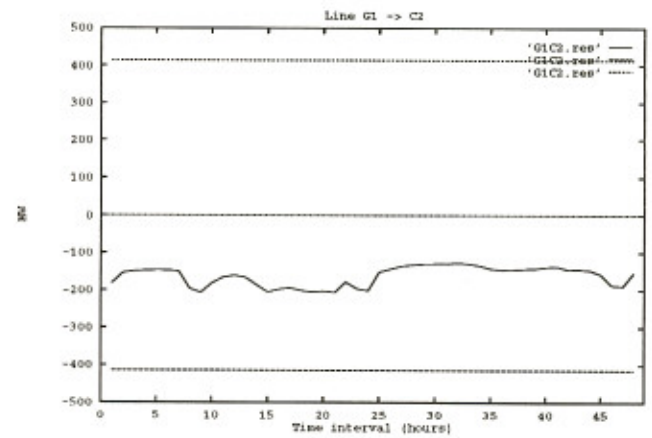
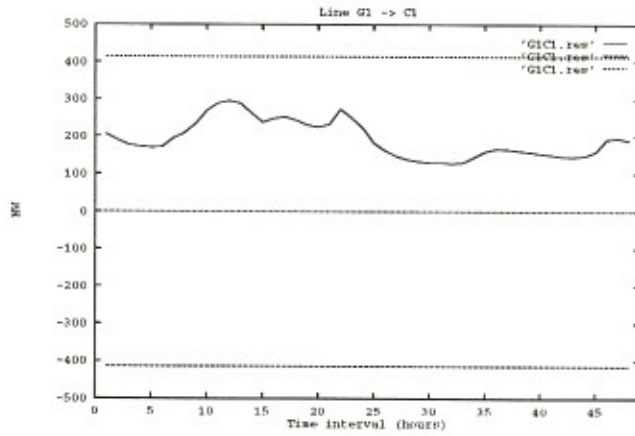


B48x : THERMAL UNITS

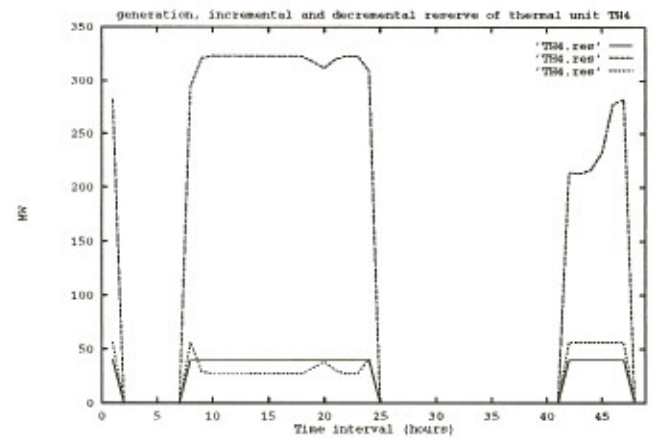
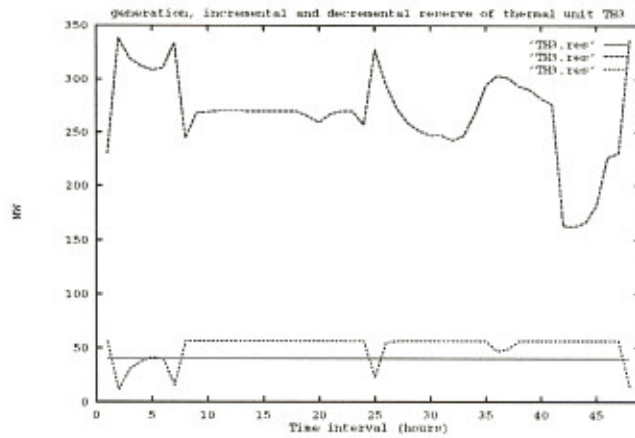
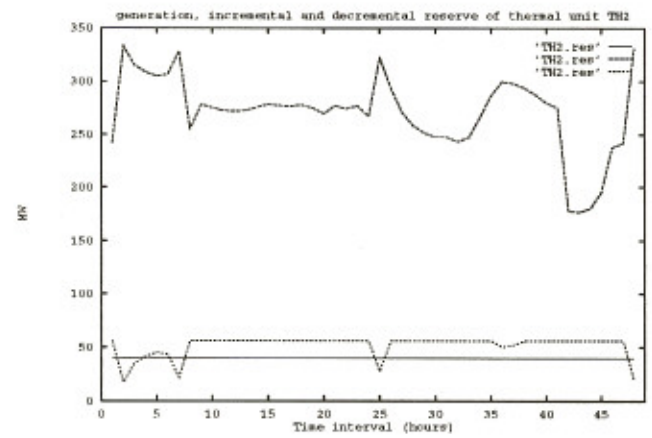
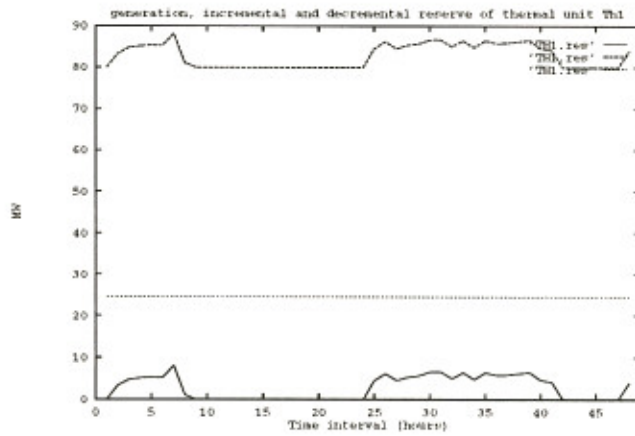
~B48x with constant efficiency



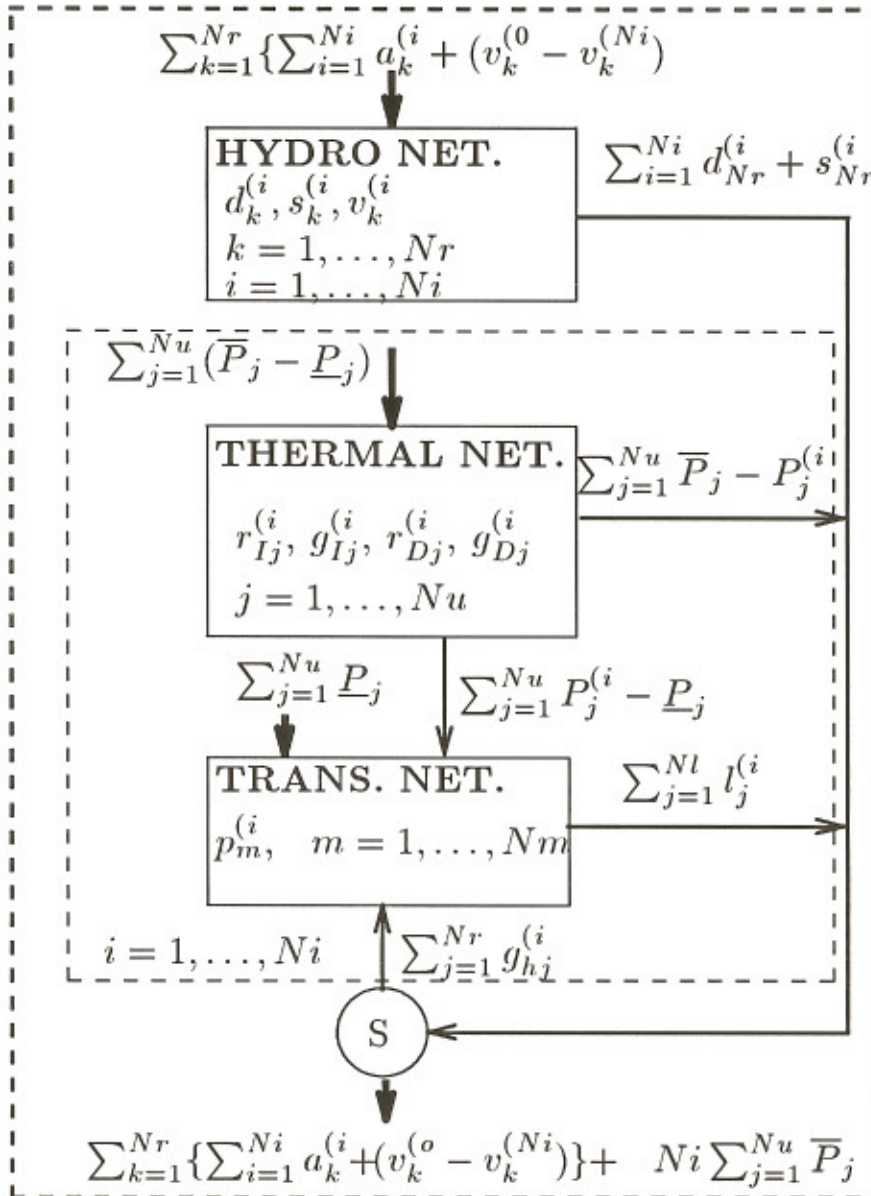
~B48x : transmission lines



~ B48x : thermal units



HTTEN



Network model vs. non-network model

- **Network model :**

$$* \left. \begin{array}{l} r_{Ij} \leq \bar{r}_{Ij} \\ g_{Ij} \\ r_{Dj} \leq \bar{r}_{Dj} \\ g_{Dj} \end{array} \right\} \rightarrow \boxed{4 \text{ variables}}$$

$$* r_{Ij} + g_{Ij} + r_{Dj} + g_{Dj} = \bar{P}_j - \underline{P}_j \rightarrow \boxed{1 \text{ network constraint}}$$

- **Non network model :**

$$* \left. \begin{array}{l} r_{Ij} \leq \bar{r}_{Ij} \\ r_{Dj} \leq \bar{r}_{Dj} \\ P_j \end{array} \right\} \rightarrow \boxed{3 \text{ variables}}$$

$$* \left. \begin{array}{l} r_{Ij} \leq \bar{P}_j - P_j \\ r_{Dj} \leq P_j - \underline{P}_j \end{array} \right\} \rightarrow \boxed{2 \text{ side constraint}}$$

ITERATIVE SOLUTION METHOD

0 Initializations.

- 0.1** Definition of the network equations of (NNLC)⁰
- 0.2** Selection of the initial solution $[x]^0$; $k := 1$.
- 0.3** Loose optimality tolerance : $\epsilon_o = 0.01$
- 0.4** Maximum hydrogeneration error : $\epsilon_L \approx 0.02$

1 Main loop.

- 1.5** k^{th} linearization : (NNLC)^k.
 Computation of λ^k at $[x]^{k-1}$.
 Computation of $[\bar{H}^{(i)}]^k$ at $[x]^{k-1}$.
 Definition of the s.c. of (NNLC)^k.
 - 1.6** k^{th} optimization : $[x]^k \xleftarrow{\text{NOXCB}}$ (NNLC)^k.
 - 1.7** If $|[H_L^{(i)}]^k - [H^{(i)}]^k| < \epsilon_L L^{(i)}, \forall i$ then
 Tight optimality tolerance $\epsilon_o := 10^{-6}$
 Final optimization : $x^* \xleftarrow{\text{NOXCB}}$ (NNLC)^k from $[x]^k$.
 If $|[H_L^{(i)}]^* - [H^{(i)}]^*| < \epsilon_L L^{(i)}, \forall i$: END
 $[x]^k := x^*$
 - 1.8** $k := k + 1$. go to **1.5** .
-